Net 426-Gb/s and 11.83-b/s/Hz 80-km Transmission with an Integrated SiP Dual-Polarization Direct Detection Receiver

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Abstract We experimentally demonstrate a single-wavelength 528-Gb/s dual-polarization OFDM 16-QAM signal transmission over an 80-km SMF with a silicon photonic dual-polarization carrier-assisted differential detection receiver, which achieves the record 426-Gb/s net data rate and 11.83-b/s/Hz net ESE for an integrated direct detection receiver. ©2023 The Author(s)

Introduction
The ever-increasing data traffic demand driven by emerging applications has propelled the optical communications research towards higher data rates. For short-reach interconnect scenarios, an important consideration is to maintain a low cost, which can be addressed by introducing emerging photonic integration techniques [1-2]. Low-cost and compact photonic integrated transceivers beyond 400G play a significant role for future 800 GE or 1.6 TbE.

Compared to a direct detection (DD) receiver, a coherent receiver exhibits a higher capacity and better tolerance to optical impairments, originating from its field recovery capability relying on a narrow-linewidth local oscillator (LO). By leveraging the photonic integration techniques, the footprint and power consumption of a coherent receiver has been dramatically reduced, which opens the door for its application in cost-sensitive short-reach scenarios. However, the fabrication of the narrow-linewidth integrated laser remains the key challenge for a monolithic integrated coherent receiver due to the material incompatibility. Additionally, the precise wavelength alignment between transceiver lasers increases the implementation cost.

Consequently, integrated LO-free DD receivers have drawn tremendous interest in cost-effective short-reach scenarios. As a conventional DD receiver offers limited sensitivity and electrical spectral efficiency (ESE), a variety of advanced DD schemes have been demonstrated to improve the overall performance of the DD. In [3-4], a silicon photonic (SiP) carrier-assisted differential detection (CADD) receiver was fabricated to achieve the transmission of net 182-Gb/s over 80-km single-mode fiber (SMF) with a net ESE of 5.2-b/s/Hz. In [5], net 258-Gb/s and net 5.31-b/s/Hz ESE transmission over 40-km SMF was presented using a SiP phase diversity receiver. To satisfy the growing capacity demand beyond 400G/λ, it is highly desirable to take advantage of polarization diversity in a similar manner to high-rate coherent technology, and explore the four-dimension (intensity and phase in dual polarization) integrated dual-polarization (DP) DD receivers.

In this paper, we demonstrate beyond 400G transmission using an integrated SiP DP-CADD receiver, which is the first on-chip DD receiver with field recovery capability of a four-dimensional complex-valued DSB signal, as a DP-coherent receiver does. A low-cost automated silicon polarization controller (ASPC) is implemented for polarization tracking, followed by two single-polarization CADD receivers for signal reception. The DP complex-valued DSB signal can be successfully detected without needing for an LO which is indispensable in a coherent receiver. In the experiment, a 528-Gb/s OFDM 16-QAM signal with a 36-GHz electrical bandwidth is successfully transmitted over 80-km SMF. Considering the 24% SD-FEC threshold [6], the net data rate and net ESE are 426 Gb/s and 11.83 b/s/Hz, respectively. Fig. 1 summarizes the recent progresses for integrated DD receivers [3-5, 7-11]. To our best knowledge, we achieve the highest capacity and ESE for an integrated DD receiver.

![Fig. 1: Recent progresses for integrated DD receivers.](image-url)
DP-CADD Receiver Design and Fabrication

Fig. 2(a) presents the schematic of the DP-CADD receiver, with the 3-D illustration of the integrated DP-CADD receiver given in Fig. 2(b). Since the state of polarization of the DP-signal varies randomly during fiber transmission, the carrier may suffer from the polarization fading issue [12]. Therefore, an ASPC is implemented to adjust the polarization automatically. The ASPC consists of the integrated polarization tuning units [13] and off-chip control circuits shown in Fig. 2(d). Firstly, the input light is separated into TE and TM portions using a polarization splitter and rotator (PSR), with the TM portion rotated to the TE light simultaneously. Then, a balanced Mach-Zehnder interferometer (MZI) is applied to split the signal into two polarizations with equal power at its output, which is realized by tuning the thermal phase shifters automatically using the off-chip control circuits. Finally, the outputs of the ASPC are detected with two integrated single-polarization CADD receivers, which consist of optical couplers, optical delay lines, 90-degree optical hybrids and several photodiodes (PDs) [14]. Fig. 2(c) gives the optical microscopy image of the fabricated SiP DP-CADD receiver with a footprint of ~1.8 mm × 1.0 mm. An edge coupler with ~4 dB/facet insertion loss is used to couple the random polarized light into the chip. We design the optical delay as 23 ps. The on-chip PD, with a 38-GHz 6-dB bandwidth at –2 V bias, was biased at –4 V for high-capacity transmission. Fig. 2(e) shows the test platform of the silicon chip. The devices were fabricated on a 220-nm commercial silicon-on-insulator (SOI) wafer with a standard CMOS manufacturing process.

Experimental Setup and DSP flow charts

Fig. 3 shows the experimental setup and DSP flow charts. At the transmitter side, a 15-kHz external cavity laser (ECL) is used as the light source, and the 528-Gb/s OFDM 16-QAM signal is generated with a 100-GSa/s digital-to-analog converter (DAC) (Micram DAC4). The modulated carrier-suppressed optical signal enters a...
polarization emulator, which consists of the optical couplers, optical delay line, and polarization beam combiner. Then, an optical coupler is used to combine the DP-signal with the carrier. After being amplified by an erbium-doped fiber amplifier (EDFA), the carrier-assisted DP-signal is launched into an 80-km fiber link. At the receiver side, another EDFA is used to amplify the signal, which is then coupled into the silicon chip and detected with the SiP DP-CADD receiver. The inset (i) plots the optical spectra in the transmission case. The electrical bandwidth of the 528-Gb/s signal is 36 GHz, with a 3-GHz guard band inserted between the carrier and sideband to combat the severe signal-signal beat interference (SSBI) enhancement [14]. The electrical spectra detected with single-ended PD of X and Y polarizations are shown in the inset (ii), respectively. Finally, the detected photocurrents are sampled by an 80-GSa/s digital storage oscilloscope (DSO) (LeCroy 36Zi-A). The transceiver DSP algorithms are also provided in Fig. 3. The transmitter DSP includes emphasis and peak-to-average-power ratio clipping. At the receiver, MIMO processing of two polarization signals is used for polarization demultiplexing. Then, equalization, single-stage SSBI cancellation, and BER calculation are employed in each polarization.

Results and Discussion
We firstly verify the feasibility of the ASPC in the experiment. Fig. 4 demonstrates the automated polarization tuning progress. The voltages are obtained based on the photocurrents detected by monitored PD1 and PD2 in Fig. 2(a). When the ASPC is disabled, the random polarization shift causes significant power difference between two polarizations, leading to a channel singularity. After the ASPC is switched on, equal optical power at two outputs can be obtained, and the signals of both polarizations are successfully recovered as shown. Note that the burr of waveform is mainly caused by the circuit noise which can be reduced with circuit optimization.

![Fig. 4: On-chip automated polarization tuning progress and the recovered constellations in different states.](image)

Fig. 5 presents the BER results at different CSPR conditions. As shown, in the back-to-back (B2B) and 80-km SMF transmission cases, the optimal CSPRs are both 13 dB, which is a trade-off between the linear beating term and effective signal powers. Finally, we measure the receiver sensitivity by varying the variable optical attenuator (VOA) at the receiver in two cases. It can be observed in Fig. 6 that the BER of 528-Gb/s OFDM 16-QAM signal after 80-km SMF transmission is below the 24% SD-FEC threshold of 4.5e-2 [6]. The insets (i-iv) illustrate the recovered constellations of X and Y polarizations at −9-dB ROP in the B2B case and transmission cases, respectively.

![Fig. 5: BER vs. CSPR in both B2B and transmission cases.](image)

Conclusions
In conclusion, we have demonstrated an integrated SiP DP-CADD receiver. A 528-Gb/s OFDM 16-QAM signal is successfully recovered after transmitted over 80-km SMF, achieving the highest 426-Gb/ net data rate and the highest 11.83-b/s/Hz net ESE for an integrated DD receiver, to the best of our knowledge. We believe that the demonstration of the high-capacity and high-ESE LO-free integrated receiver provides a promising low-cost solution for next-generation data center interconnects and short-reach communications.
References


